

# The fission rate in multi-dimensional Langevin calculations

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# Motivation

Understanding of collective properties of nuclei

Large difference in the predictions of dissipation properties in different theoretical models

Experimental data on nuclear dissipation have often been interpreted using one-dimensional model calculations of the Langevin or Fokker-Planck type.

Investigate the influence of the dimensionality of the deformation space on the fission process in Langevin calculations.

# Theoretical description of fission

## stochastic approach

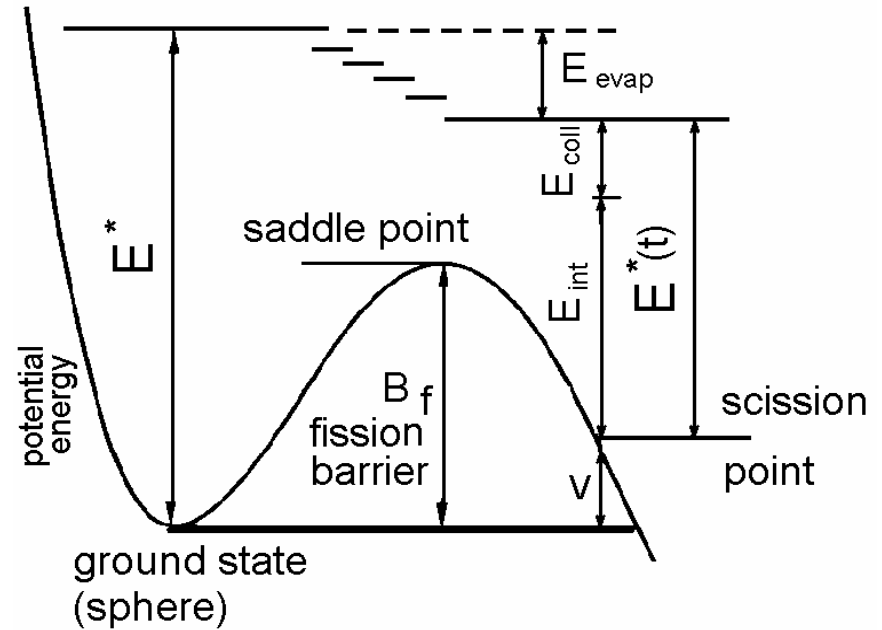
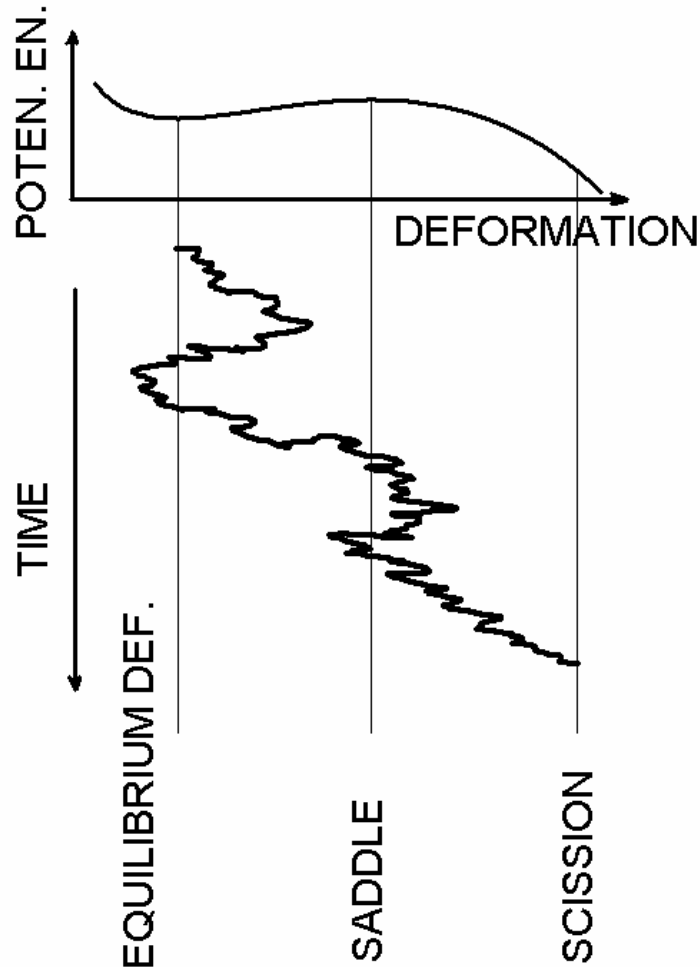
collective variables  
(shape of the nucleus)

internal degrees of freedom  
("heat bath")

## Langevin equations

Langevin equations describe time evolution of the collective variables like the evolution of Brownian particle that interacts stochastically with a "heat bath".

# The stochastic approach



$E_{\text{coll}}$  - the energy connected with collective degrees of freedom

$E_{\text{int}}$  - the energy connected with internal degrees of freedom

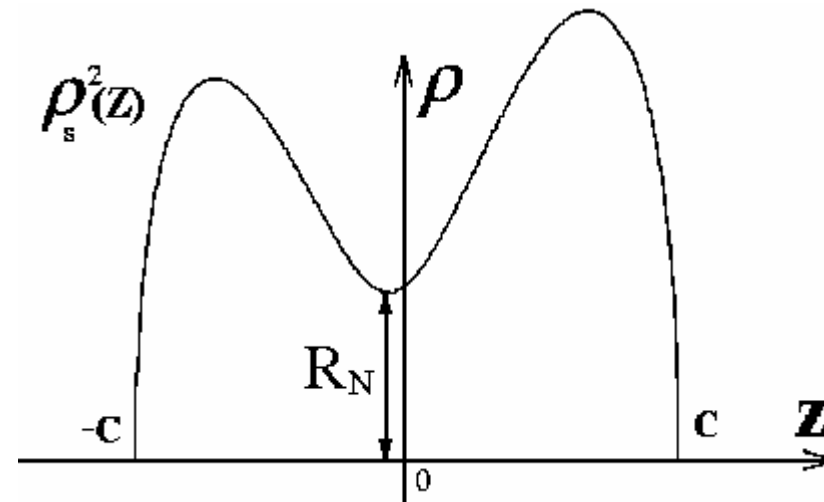
$E_{\text{evap}}$  - the energy carried away by the evaporated particles

# The (c,h,a)-parameterization

$$\rho_s^2(z) = \begin{cases} (c^2 - z^2) (A_s + Bz^2/c^2 + \alpha z/c), & \text{if } B \geq 0; \\ (c^2 - z^2) (A_s + \alpha z/c) \exp(Bcz^2), & \text{if } B < 0, \end{cases}$$

$$B = 2h + \frac{c-1}{2}.$$

$$A_s = \begin{cases} c^{-3} - \frac{B}{5}, & \text{if } B \geq 0; \\ -\frac{4}{3} \frac{B}{\exp(Bc^3) + \left(1 + \frac{1}{2Bc^3}\right) \sqrt{-\pi Bc^3} \operatorname{erf}(\sqrt{-Bc^3})}, & \text{if } B < 0. \end{cases}$$



# The Langevin equations

$$\dot{q}_i = \mu_{ij} p_j,$$

$$\dot{p}_i = -\frac{1}{2} p_i p_k \frac{\partial \mu_{jk}}{\partial q_i} - \frac{\partial F}{\partial q_i} - \gamma_{ij} \mu_{jk} p_k + \theta_{ij} \xi_j(t)$$

**q** - collective coordinate **p** - conjugate momentum

$\mathbf{m}_{ij} (\|\mu_{ij}\| = \|\mathbf{m}_{ij}\|^{-1})$  - inertia tensor

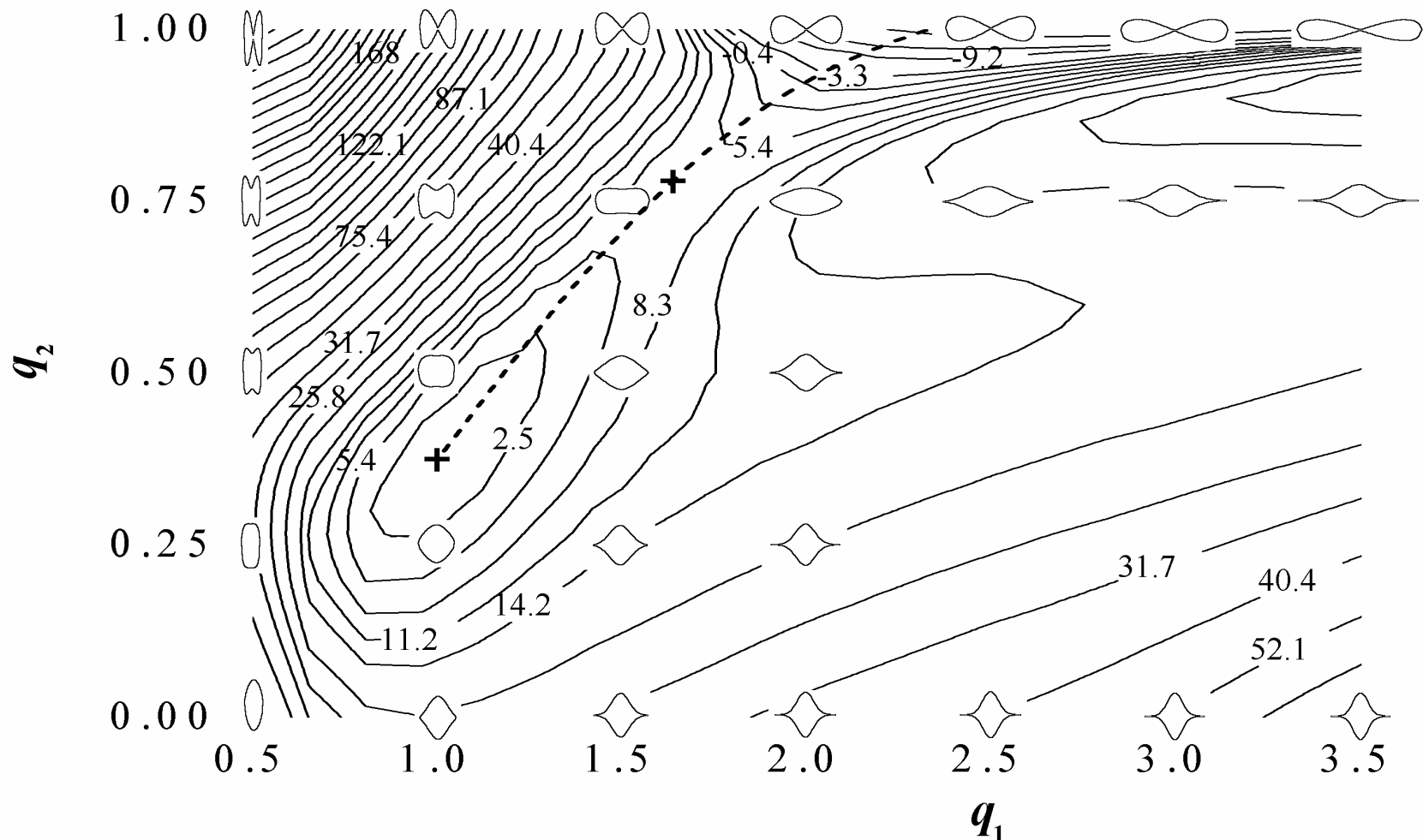
$F(\mathbf{q}) = V(\mathbf{q}) - a(\mathbf{q})T^2$  - Helmholtz free energy

$a(\mathbf{q})$  - level density       $T$  - temperature

$V$  - potential energy       $\gamma_{ij}$  - friction tensor

$\theta_{ij} \xi_j$  - random force       $\xi_j$  - random variable

# The collective coordinates



$$q_1 = c;$$

$$q_2 = (h+1.5)/(h_{sc}+1.5);$$

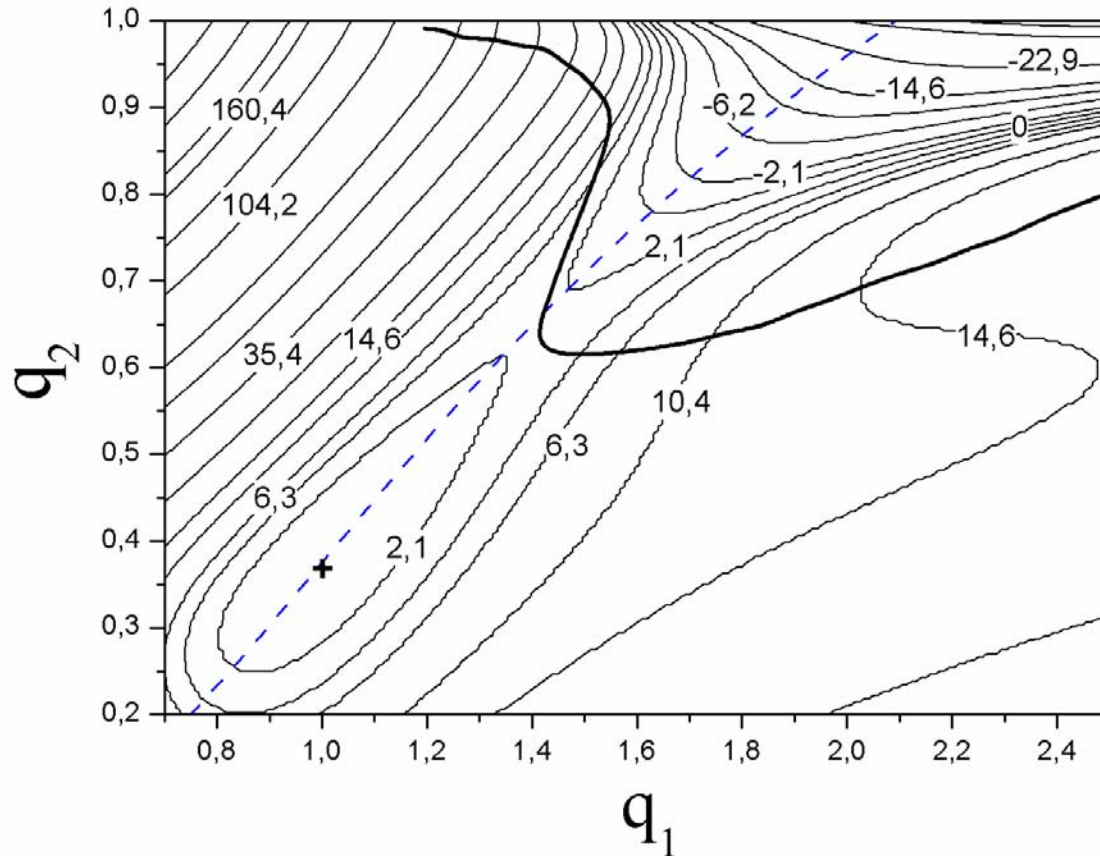
$$h_{sc} = 5/(2c^3) + (1-c)/4;$$

$$q_3 = \alpha/(As+B) \text{ if } B \geq 0$$

$$q_3 = \alpha/As \text{ if } B < 0$$

Nadtochy and Adeev PRC, 2005

# The collective coordinates



The potential energy for the  $^{248}\text{Cf}$ .

The solid curve – saddle point configurations.

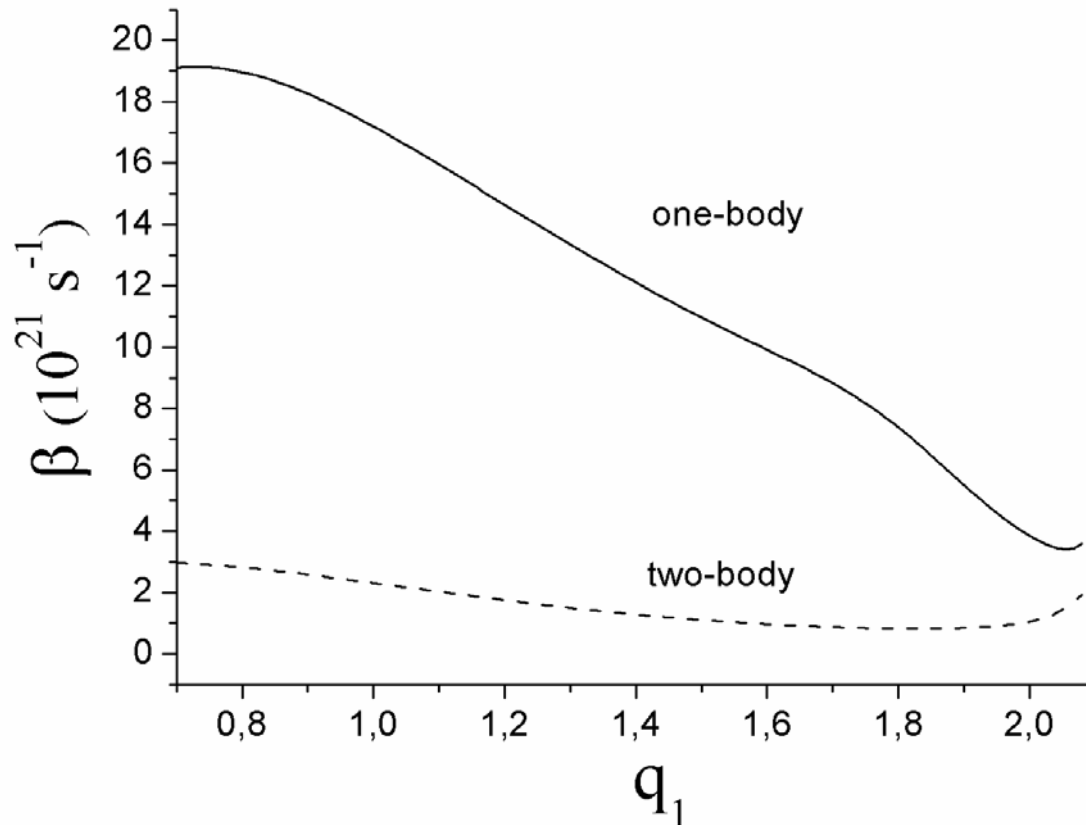
The dashed curve – fission valley.

Calculations:

1. **One – dimensional** (bottom of fission valley)  $h=a=0$
2. **Two – dimensional** (symmetrical fission)  $q_3=0$ ,  $\mathbf{q}=(q_1, q_2)$
3. **Three – dimensional**  $\mathbf{q}=(q_1, q_2, q_3)$ .

# The friction parameter

The friction parameter  
 $\beta = \gamma/m$



- **One-body dissipation**  
(“wall” and “wall-plus-window” formulas)
- **Two-body dissipation** with the two-body friction constant  
 $v_0 = 2 \times 10^{-23} \text{ MeV s fm}^{-3}$

# Results of calculations

1-, 2-, and 3-dimensional

calculations for

$^{248}\text{Cf}$  at  $E^* = 30 \text{ MeV}$  and  $E^* = 150 \text{ MeV}$ ;

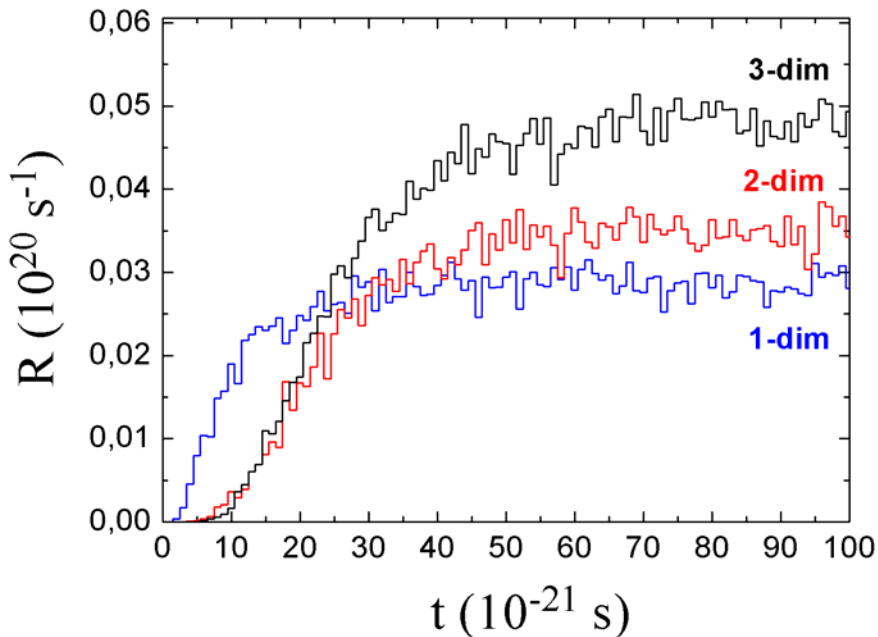
$^{213}\text{At}$  at  $E^* = 190 \text{ MeV}$

Fission rate:  $R(t) = -1/N(t) \, dN(t)/dt$

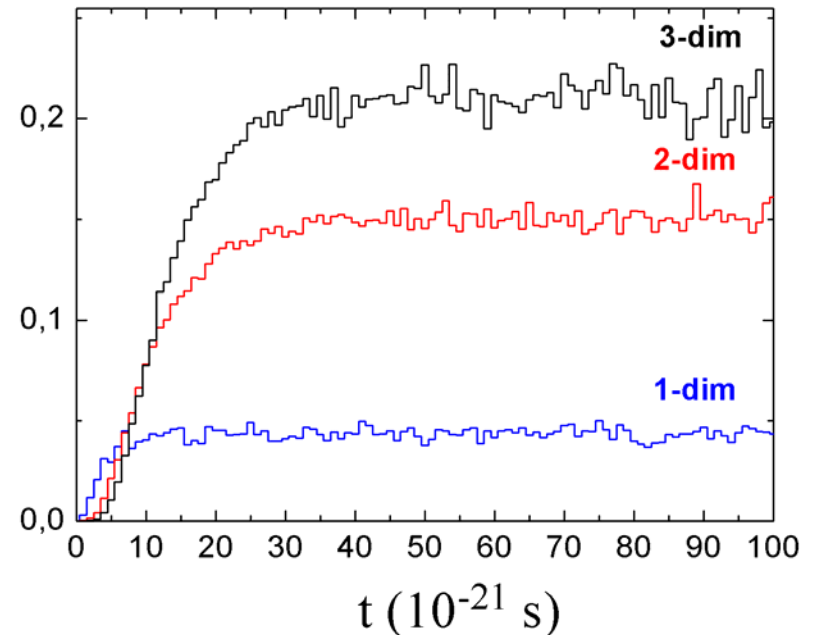
$N(t)$  - the number of Langevin trajectories, which did not escape beyond the saddle at time  $t$ .

# The results for the $^{248}\text{Cf}$ (one-body)

$E^*=30 \text{ MeV}$



$E^*=150 \text{ MeV}$



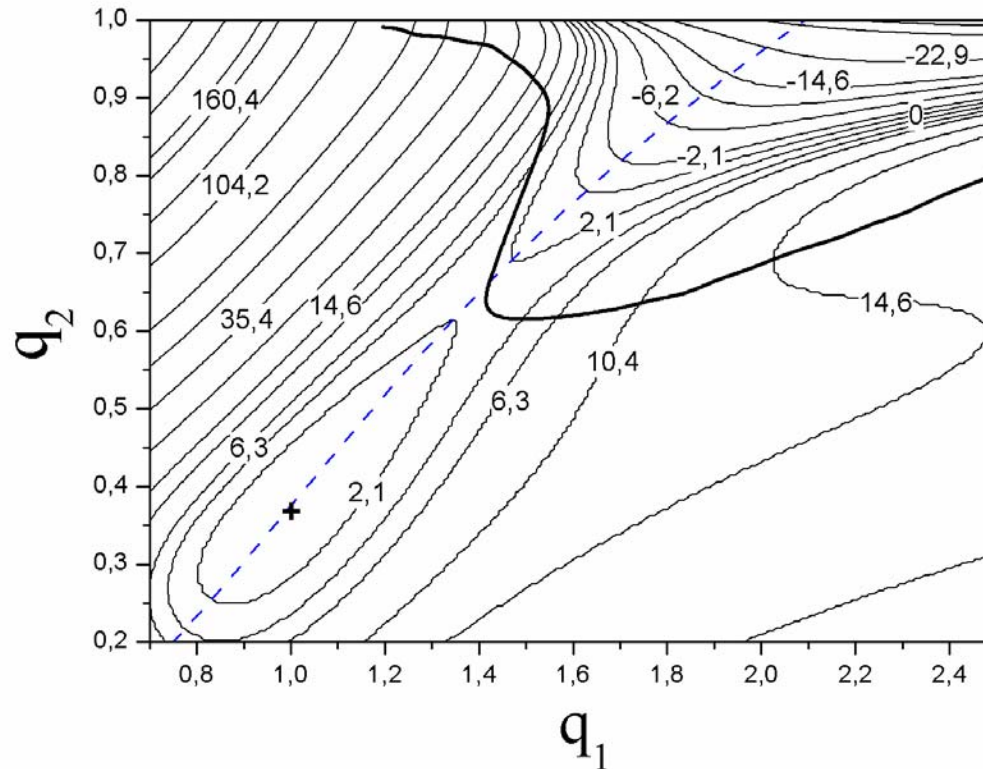
The stationary values:

$$R^{3d}/R^{1d} = 1.8$$

$$R^{3d}/R^{1d} = 5$$

The lowest transient time – one-dimensional calculations

# The results for the $^{248}\text{Cf}$



one-dimensional case:

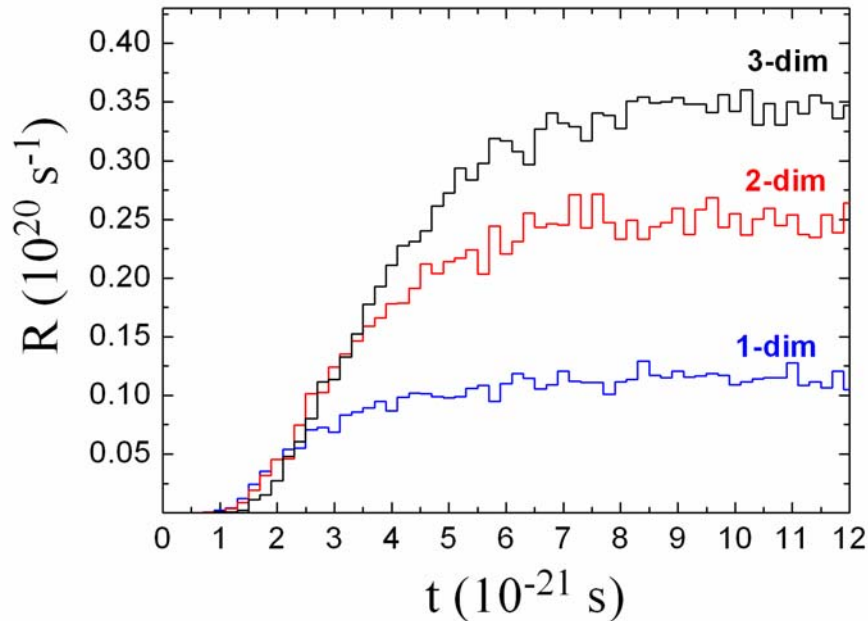
$R(t)$  - flux over only  
saddle point

multi-dimensional case:

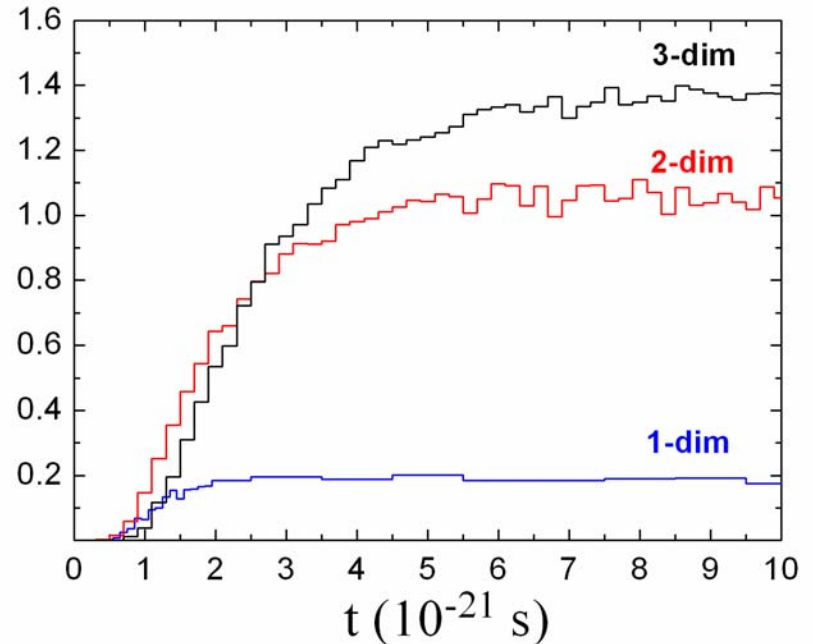
$R(t)$  - flux over populated  
saddle point configurations

# The results for the $^{248}\text{Cf}$ (two-body)

$E^*=30 \text{ MeV}$



$E^*=150 \text{ MeV}$



The stationary values:

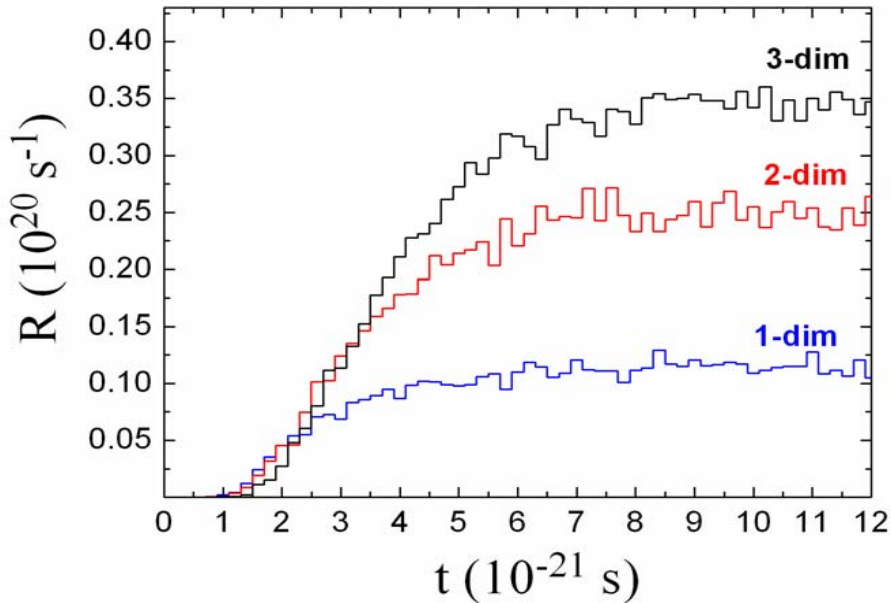
$$R^{3d}/R^{1d} = 3$$

$$R^{3d}/R^{1d} = 8$$

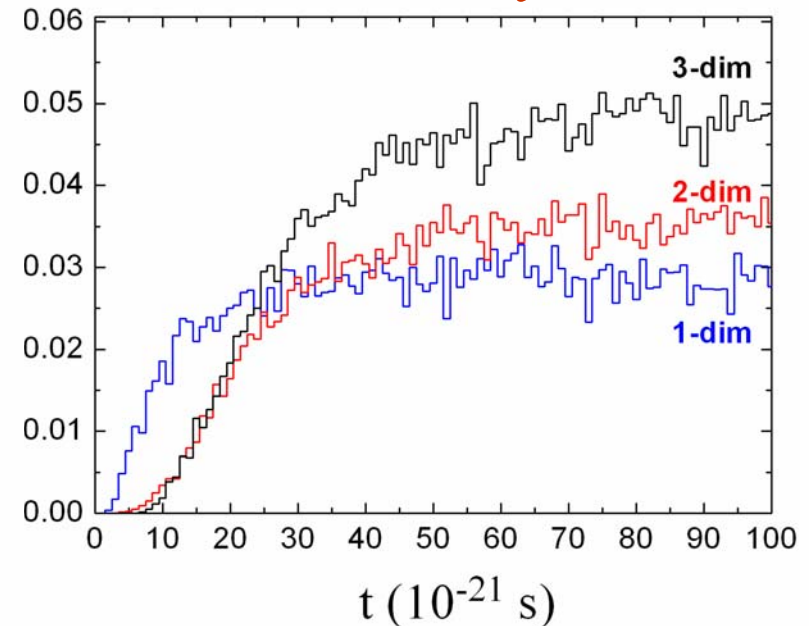
The lowest transient time – one-dimensional calculations

# The results for the $^{248}\text{Cf}$ for $E^*=30\text{MeV}$

two-body



one-body



The collective energy at saddle point configurations averaged over Langevin trajectories :

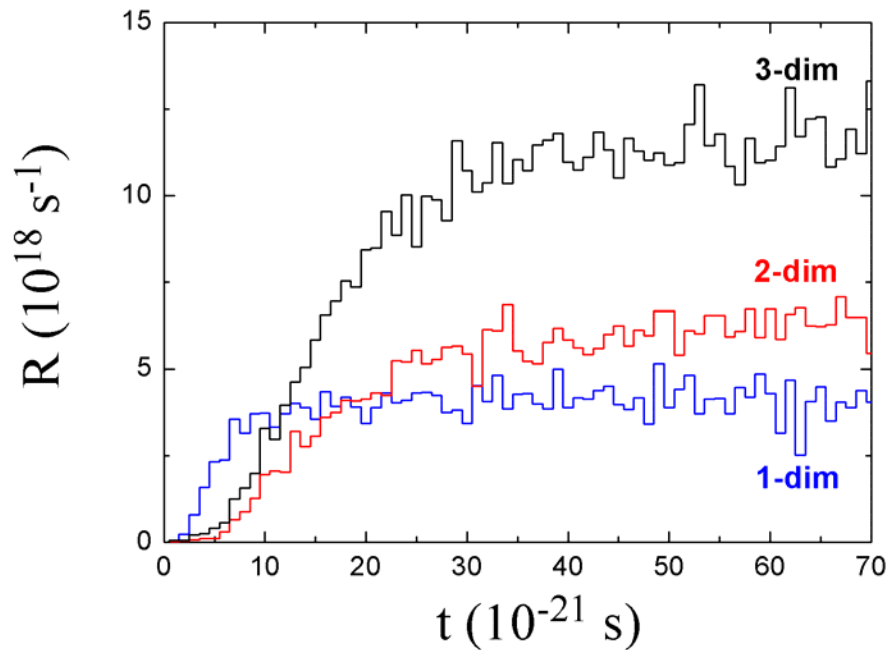
two-body

1d:  $\langle E_{\text{coll}} \rangle = 1.43 \text{ MeV}$   
2d:  $\langle E_{\text{coll}} \rangle = 2.58 \text{ MeV}$   
3d:  $\langle E_{\text{coll}} \rangle = 3.60 \text{ MeV}$

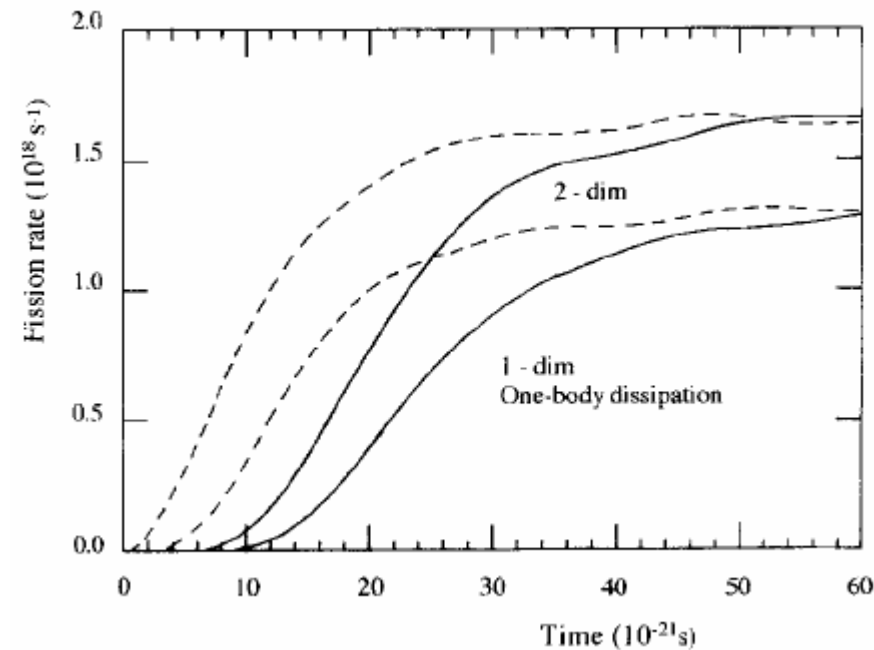
one-body

1d:  $\langle E_{\text{coll}} \rangle = 1.26 \text{ MeV}$   
2d:  $\langle E_{\text{coll}} \rangle = 2.07 \text{ MeV}$   
3d:  $\langle E_{\text{coll}} \rangle = 2.65 \text{ MeV}$

# The results for the $^{213}\text{At}$ (one-body)



present calc.



Abe et. al. Phys. Rep. (1996)

1-dimensional versus 2-dimensional:

The same qualitative results for the stationary values,  
but different behavior for transient times.

# Summary

- The results of  $R(t)$  calculations appreciable dependent on the number of collective coordinates involved in Langevin calculations.
- The transient time and stationary value of fission rate is larger in multi-dimensional calculations than in one-dimensional calculations.
- How the introduction of another collective coordinates will influence on the  $R(t)$ ?